AD NO. ___________________________
DTC PROJECT NO. 8-CO-160-UXO-021
REPORT NO. ATC-9743

STANDARDIZED

UXO TECHNOLOGY DEMONSTRATION SITE

BLIND GRID SCORING RECORD NO. 898

SITE LOCATION:
U.S. ARMY ABERDEEN PROVING GROUND

DEMONSTRATOR:
SKY RESEARCH, INC.
445 DEAD INDIAN MEMORIAL ROAD
ASHLAND, OR 97520

TECHNOLOGY TYPE/PLATFORM:
EM61 MKII/PUSHCART

PREPARED BY:
U.S. ARMY ABERDEEN TEST CENTER
ABERDEEN PROVING GROUND, MD 21005-5059

JULY 2008

Prepared for:
U.S. ARMY ENVIRONMENTAL COMMAND
ABERDEEN PROVING GROUND, MD 21010-5401

U.S. ARMY DEVELOPMENTAL TEST COMMAND
ABERDEEN PROVING GROUND, MD 21005-5055

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J. Stephen McClung	[signature]	July 2008
NAME (Printed)	SIGNATURE	DATE

CONCURRENCE:	NAME (Printed)	SIGNATURE	DATE
Program Mgr/Customer (If not ATC owned technology)	Patrick McDonnell	Patrick McDonnell	8/4/08
Directorate Director	Charles Valz	C Valz	8/6/08
Directorate OPSEC QC and Team Leader	William Burch	William Burch	23 JUL 08
ATC OPSEC Officer/ Security Manager	Jenell Bigham	Jenell Bigham	26 Aug 08
Public Affairs Specialist	Crystal Maynard	C Maynard	26 Aug 08
Technical Director, ATC	John R. Wallace	John R. Wallace	2 Sep 08
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Commander
U.S. Army Aberdeen Test Center
ATTN: TEDT-AT-SLE
Aberdeen Proving Ground, MD 21005-5059

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Commander
U.S. Army Environmental Command
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14. ABSTRACT

This scoring record documents the efforts of Sky Research, Inc. to detect and discriminate inert unexploded ordnance (UXO) utilizing the APG Standardized UXO Technology Demonstration Site Blind Grid Field. This Scoring Record was coordinated by William Burch and the Standardized UXO Technology Demonstration Site Scoring Committee. Organizations on the committee include the U.S. Army Corps of Engineers, the Environmental Security Technology Certification Program, the Strategic Environmental Research and Development Program, the Institute for Defense Analysis, the U.S. Army Environmental Command, and the U.S. Army Aberdeen Test Center.

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Authors:

Rick Fling
Aberdeen Test Support Services (ATSS)
Sverdrup Technology, Inc.
U.S. Army Aberdeen Proving Ground (APG)

Christina McClung
Aberdeen Data Services Team (ADST)
Logistics Engineering and Information Technology Company (Log.Sec)
U.S. Army Aberdeen Proving Ground

Contributors:

William Burch
Military Environmental Technology Demonstration Center (METDC)
U.S. Army Aberdeen Test Center (ATC)
U.S. Army Aberdeen Proving Ground

Leonardo Lombardo
Aberdeen Test Support Services
Sverdrup Technology, Inc.
U.S. Army Aberdeen Proving Ground

Patrick McDonnell
Booz Allen Hamilton (BAH)
U.S. Army Environmental Command (USAEC)
U.S. Army Aberdeen Proving Ground

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SECTION 1. GENERAL INFORMATION

1.1 BACKGROUND

Technologies under development for the detection and discrimination of munitions and explosives of concern (MEC) - i.e. unexploded ordnance (UXO) and discarded military munitions (DMM) require testing so that their performance can be characterized. To that end, Standardized Test Sites have been developed at Aberdeen Proving Ground (APG), Maryland, and U.S. Army Yuma Proving Ground (YPG), Arizona. These test sites provide a diversity of geology, climate, terrain, and weather as well as diversity in ordnance and clutter. Testing at these sites is independently administered and analyzed by the government for the purposes of characterizing technologies, tracking performance with system development, comparing performance of different systems, and comparing performance in different environments.

The Standardized UXO Technology Demonstration Site Program is a multiagency program spearheaded by the U.S. Army Environmental Command (USAEC). The U.S. Army Aberdeen Test Center (ATC) and the U.S. Army Corps of Engineers Engineer Research and Development Center (ERDC) provide programmatic support. The program is being funded and supported by the Environmental Security Technology Certification Program (ESTCP), the Strategic Environmental Research and Development Program (SERDP), and the Army Environmental Quality Technology Program (EQT).

1.2 SCORING OBJECTIVES

The objective in the Standardized UXO Technology Demonstration Site Program is to evaluate the detection and discrimination capabilities of a given technology under various field and soil conditions. Inert munitions and clutter items are positioned in various orientations and depths in the ground.

The evaluation objectives are as follows:

a. To determine detection and discrimination effectiveness under realistic scenarios that may vary targets, geology, clutter, topography, and vegetation.

b. To determine cost, time, and manpower requirements to operate the technology.

c. To determine demonstrator's ability to analyze survey data in a timely manner and provide prioritized "Target Lists" with associated confidence levels.

d. To provide independent site management to enable the collection of high quality, ground-truth, geo-referenced data for post-demonstration analysis.

1.2.1 Scoring Methodology

a. The scoring of the demonstrator's performance is conducted in two stages. These two stages are termed the RESPONSE STAGE and DISCRIMINATION STAGE. For both stages, the probability of detection (P_d) and the false alarms are reported as receiver-operating

characteristic (ROC) curves. False alarms are divided into those anomalies that correspond to emplaced clutter items, measuring the probability of false positive (P_{fp}) and those that do not correspond to any known item, termed background alarms.

b. The RESPONSE STAGE scoring evaluates the ability of the system to detect emplaced targets without regard to ability to discriminate ordnance from other anomalies. For the blind grid RESPONSE STAGE, the demonstrator provides the scoring committee with a target response from each and every grid square along with a noise level below which target responses are deemed insufficient to warrant further investigation. This list is generated with minimal processing and, since a value is provided for every grid square, will include signals both above and below the system noise level.

c. The DISCRIMINATION STAGE evaluates the demonstrator's ability to correctly identify ordnance as such and to reject clutter. For the blind grid DISCRIMINATION STAGE, the demonstrator provides the scoring committee with the output of the algorithms applied in the discrimination-stage processing for each grid square. The values in this list are prioritized based on the demonstrator's determination that a grid square is likely to contain ordnance. Thus, higher output values are indicative of higher confidence that an ordnance item is present at the specified location. For digital signal processing, priority ranking is based on algorithm output. For other discrimination approaches, priority ranking is based on human (subjective) judgment. The demonstrator also specifies the threshold in the prioritized ranking that provides optimum performance, (i.e. that is expected to retain all detected ordnance and rejects the maximum amount of clutter).

d. The demonstrator is also scored on EFFICIENCY and REJECTION RATIO, which measures the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of ordnance detections from the anomaly list, while rejecting the maximum number of anomalies arising from non-ordnance items. EFFICIENCY measures the fraction of detected ordnance retained after discrimination, while the REJECTION RATIO measures the fraction of false alarms rejected. Both measures are defined relative to performance at the demonstrator-supplied level below which all responses are considered noise, i.e., the maximum ordnance detectable by the sensor and its accompanying false positive rate or background alarm rate.

e. All scoring factors are generated utilizing the Standardized UXO Probability and Plot Program, version 3.1.1.

1.2.2 <u>Scoring Factors</u>

Factors to be measured and evaluated as part of this demonstration include:

a. Response Stage ROC curves:

(1) Probability of Detection (P_d^{res}).

(2) Probability of False Positive (P_{fp}^{res}).

(3) Background Alarm Rate (BAR^{res}) or Probability of Background Alarm (P_{BA}^{res}).

b. Discrimination Stage ROC curves:

(1) Probability of Detection (P_d^{disc}).

(2) Probability of False Positive (P_{fp}^{disc}).

(3) Background Alarm Rate (BAR^{disc}) or Probability of Background Alarm (P_{BA}^{disc}).

c. Metrics:

(1) Efficiency (E).

(2) False Positive Rejection Rate (R_{fp}).

(3) Background Alarm Rejection Rate (R_{BA}).

d. Other:

(1) Probability of Detection by Size and Depth.

(2) Classification by type (i.e., 20-mm, 40-mm, 105-mm, etc.).

(3) Location accuracy.

(4) Equipment setup, calibration time and corresponding man-hour requirements.

(5) Survey time and corresponding man-hour requirements.

(6) Reacquisition/resurvey time and man-hour requirements (if any).

(7) Downtime due to system malfunctions and maintenance requirements.

1.3 STANDARD AND NONSTANDARD INERT ORDNANCE TARGETS

The standard and nonstandard ordnance items emplaced in the test areas are listed in Table 1. Standardized targets are members of a set of specific ordnance items that have identical properties to all other items in the set (caliber, configuration, size, weight, aspect ratio, material, filler, magnetic remanence, and nomenclature). Nonstandard targets are ordnance items having properties that differ from those in the set of standardized targets.

TABLE 1. INERT ORDNANCE TARGETS

Standard Type	Nonstandard (NS)
20-mm Projectile M55	20-mm Projectile M55
	20-mm Projectile M97
40-mm Grenades M385	40-mm Grenades M385
40-mm Projectile MKII Bodies	40-mm Projectile M813
BDU-28 Submunition	
BLU-26 Submunition	
M42 Submunition	
57-mm Projectile APC M86	
60-mm Mortar M49A3	60-mm Mortar (JPG)
	60-mm Mortar M49
2.75-inch Rocket M230	2.75-inch Rocket M230
	2.75-inch Rocket XM229
MK 118 ROCKEYE	
81-mm Mortar M374	81-mm Mortar (JPG)
	81-mm Mortar M374
105-mm HEAT Rounds M456	
105-mm Projectile M60	105-mm Projectile M60
155-mm Projectile M483A1	155-mm Projectile M483A
	500-lb Bomb
	M75 Submunition

HEAT = high-explosive antitank.
JPG = Jefferson Proving Ground.

SECTION 2. DEMONSTRATION

2.1 DEMONSTRATOR INFORMATION

2.1.1 Demonstrator Point of Contact (POC) and Address

POC: Ms. Stacey Kingsbury
(540) 961-9132

Address: Sky Research, Inc.
445 Dead Indian Memorial Road
Ashland, OR 97520

2.1.2 System Description (provided by demonstrator)

Sky Research is conducting three surveys each at APG and YPG to demonstrate the capabilities of electromagnetic induction (EMI) and magnetometer technologies and our data analysis capabilities. These three surveys include:

a. Survey 1. The active response site and the test sites (calibration lane, blind test grid, and open field scenarios) with Sky Research's EM61-MKII towed array (fig. 1). This survey utilizes an array of five Geonics EM61 MKII sensors deployed with a 0.5-meter spacing between each coil. Data are logged using the SKY-DAS at a 10 Hz rate and positioned with the Leica TPS1200 Robotic Total Station (RTS) technology. In addition, the DAS collects sensor and platform orientation data from the Crossbow AHRS-400 inertial measurement unit (IMU).

b. Survey 2. Active site and test site (calibration lanes, blind test grids, open field, wooded area, moguls, and desert extreme scenarios) with Sky Research's man-portable, quad-sensor magnetometer array; digital compass for orientation; and Leica RTS for positioning. Geometrics G-823 total field cesium vapor magnetometers are being used for this survey. Sky Research deploys this equipment on a low-noise, man-portable, quad-sensor array with an integrated digital compass for sensor orientation information. The G-823 system is configured to stream data at 10 samples per channel per second (10 Hz). At a nominal traverse rate of 0.8 meter per second (around 3 km/hr), this equates to approximately one sample per 8 cm of forward advance.

c. Survey 3. Calibration lane, blind test grids, and moguls only with Sky Research's gimbaled EM61 MKII developed via SERDP 1310. The cart is configured to mitigate motion and orientation changes and positioned with the Leica RTS. This survey deploys the same sensors as survey 1: a Geonics EM61-MKII, Crossbow IMU integrated with the Leica RTS.

Figure 1.   Demonstrator's system, EM61 MKII/pushcart.

2.1.3   Data Processing Description (provided by demonstrator)

a. In addition to standard data processing, we are demonstrating the capability to merge orientation information with sensor data, advanced electromagnetic (EM) and MAG processing capability, and the advanced capability to analyze magnetic and EM data together using the UXOLab software package. This advanced analysis includes the merging of target lists collected by each sensor system and the use of the magnetic data to constrain the EM interpretation via cooperative inversion. Sky Research's standard data processing includes data leveling, statistical data assessment, grid generation, and customized data filtering to accentuate target signatures. Sky Research uses software from the sensor manufacturers and the UXOLab software developed by the proposed project Principal Investigator, Dr. Stephen Billings, to complete all data processing tasks.

b. The discrimination methodology we deploy is a variation of the finger-printing method. That is, the response of each anomaly will be compared with the response of each item in a library of ordnance items expected to be present in the area. All inversions are performed using the full 3-D position and orientation information of each sensor.

2.1.4   Data Submission Format

Data are submitted for scoring in accordance with data submission protocols outlined in the Standardized UXO Technology Demonstration Site Handbook. These submitted data are not included in this report in order to protect ground truth information.

2.1.5 Demonstrator Quality Assurance (QA) and Quality Control (QC) (provided by demonstrator)

QC. The following procedures and logs are used to maximize standardization, repeatability, and control of mapping activities:

a. Equipment Standardization Form: This log documents the daily calibration of each field sensor and navigation system. This form documents the results and analysis of the pre- and post-survey Static Test, Static Spike Test, Cable Shake Test, Backsight, and QC Check Positions.

b. Position Standardization Form: This log will document daily calibration of the real-time kinematic (RTK) Navigation system. Pre-and post-survey results of the 3-Point Navigation Function Test, summary data sampling parameters, and detection of blind seed items are documented.

c. Survey Event Summary Form: This log is used to identify the location of each geophysical survey crew on a daily basis. The log tracks crew members, equipment, filenames, and expected areas to be surveyed. Attached to this daily log are maps of the areas to be surveyed containing the coordinates of benchmarks in the areas as well as the coordinates of each quadrant corner.

d. Data Processing Log: All data from the field are run through a standard data-processing procedure. This procedure is the same for all data and is tracked with the Data Processing Log. This log documents all coordinate transformations, visual data-quality checks, statistical data-quality checks, survey-coverage statistics, interpolation parameters, etc.

e. Target Reanalysis: All targets analyzed as part of the project are subject to review by the project geophysicist. In addition, a minimum of 10 percent of all targets are reanalyzed by a separate geophysicist to ensure data quality.

QA. QA measures are integrated with the QC activities described above in Section I1 above. In addition, standardization procedures implemented on a site-specific basis are used to maximize efficiency and to adjust to logistical and schedule requirements. The procedure below is utilized at the site to define the spatial accuracy of the data as well as the repeatability of the sensor readings:

a. A 50-foot-long straight-line transect is established with the positions of the endpoints and midpoint logged via RTS.

b. Wherever possible the traverse line is oriented North to South. Each survey system (sensor and navigation unit) used to collect data is operated over the transect each day following standard procedures as follows:

1) An operator logs background data along the traverse, first heading north from the southern endpoint, and then returning south from the northern endpoint.

2) A metallic pin-flag is placed over the midpoint.

3) The operator logs data along the same path, first traveling north, and then returning south.

4) The operator logs data along the same path, first traveling north at a slow pace, and then returning south at a significantly more rapid pace.

c. All data lines are downloaded and provided to the site geophysicist for review. These data are examined to determine the repeatability of the pin-flag anomaly amplitude and the repeatability of the positional location of the amplitude peak.

In addition, for the EM, a static background and spike test is performed twice daily, prior to collecting data and after completion of data collection. This test monitors the instrument background readings, monitors for electronic drift, identifies potential interference, and determines the impulse response and repeatability of measurements over a standard test item. The standard test item is a standard 2-inch diameter steel trailer hitch ball. For the towed array system, the tow vehicle is turned on during the test. With the instrument held in static position, measurements are recorded for at least 3 minutes. A standard test item is then placed under the center of each coil and an additional minute of data is recorded. Static background readings for the EM-61 MKII should remain within 2.5 mV of background. Readings for the response of the standard test item should be within 20 percent after subtraction of the sensor baseline response.

For the magnetometer array, a heading calibration and test is performed twice daily, prior to collecting data and after completion of data collection. This test involves traverses across a known point located away from buried UXO or other metallic debris. A 5-meter-length of line is walked in eight cardinal directions (N-S, S-N, E-W, W-E, SE-NW, NW-SE, SW-NE, NE-SW). The intersections of each line-direction and each sensor are then compared. If any sensor/line direction combination is found to differ by more than 10 nT, the survey is halted until the reason for this heading-induced error is identified and eliminated.

2.1.6 Additional Records

The following record(s) by this vendor can be accessed via the Internet as Microsoft Word documents at www.uxotestsites.org.

2.2 APG SITE INFORMATION

2.2.1 Location

The APG Standardized Test Site is located within a secured range area of the Aberdeen Area of APG. The Aberdeen Area of APG is located approximately 30 miles northeast of Baltimore at the northern end of the Chesapeake Bay. The Standardized Test Site encompasses 17 acres of upland and lowland flats, woods, and wetlands.

2.2.2 Soil Type

According to the soils survey conducted for the entire area of APG in 1998, the test site consists primarily of Elkton Series type soil (ref 2). The Elkton Series consists of very deep, slowly permeable, poorly drained soils. These soils formed in silty aeolin sediments and the underlying loamy alluvial and marine sediments. They are on upland and lowland flats and in depressions of the Mid-Atlantic Coastal Plain. Slopes range from 0 to 2 percent.

ERDC conducted a site-specific analysis in May of 2002 (ref 3). The results basically matched the soil survey mentioned above. Seventy percent of the samples taken were classified as silty loam. The majority (77 percent) of the soil samples had a measured water content between 15 and 30 percent with the water content decreasing slightly with depth.

For more details concerning the soil properties at the APG test site, go to www.uxotestsites.org on the Web to view the entire soils description report.

2.2.3 Test Areas

A description of the test site areas at APG is included in Table 2.

TABLE 2. TEST SITE AREAS

Area	Description
Calibration grid	Contains 14 standard ordnance items buried in six positions at various angles and depths to allow demonstrator equipment calibration.
Blind grid	Contains 400 grid cells in a 0.2-hectare (0.5-acre) site. The center of each grid cell contains ordnance, clutter, or nothing.

SECTION 3. FIELD DATA

3.1 DATE OF FIELD ACTIVITIES (30 and 31 January and 1, 3, and 17 February 2006)

3.2 AREAS TESTED/NUMBER OF HOURS

Areas tested and total numbers of hours operated at each site are summarized in Table 3.

TABLE 3. AREAS TESTED AND NUMBER OF HOURS

Area	Number of Hours
Calibration lanes	11.66
Blind grid	2.25

3.3 TEST CONDITIONS

3.3.1 Weather Conditions

An APG weather station located approximately 1 mile west of the test site was used to record average temperature and precipitation on a half-hour basis for each day of operation. The temperatures listed in Table 4 represent the average temperature during field operations from 0700 to 1700 hours while precipitation data represents a daily total amount of rainfall. Hourly weather logs used to generate this summary are provided in Appendix B.

TABLE 4. TEMPERATURE/PRECIPITATION DATA SUMMARY

Date, 2006	Average Temperature, ^{o}F	Total Daily Precipitation, in.
30 January	46.3	0.01
31 January	45.2	0.00
01February	41.1	0.00
02 February	58.9	0.33
17 February	53.2	0.01

3.3.2 Field Conditions

Sky Research surveyed the blind grid area 1 February 2006. The weather was cold and the field was wet during the survey.

3.3.3 Soil Moisture

Three soil probes were placed at various locations within the site to capture soil moisture data: calibration, mogul, open field, and wooded areas. Measurements were collected in percent moisture and were taken twice daily (morning and afternoon) from five different soil depths (1 to 6 in., 6 to 12 in., 12 to 24 in., 24 to 36 in., and 36 to 48 in.) from each probe. Soil moisture logs are included in Appendix C.

3.4 FIELD ACTIVITIES

3.4.1 Setup/Mobilization

These activities included initial mobilization and daily equipment preparation and break down. A three-person crew took 12 hours and 15 minutes to perform the initial setup and mobilization. There was no daily equipment preparation, and end of the day equipment break down lasted 50 minutes.

3.4.2 Calibration

Sky Research spent a total of 11 hours and 40 minutes in the calibration lanes, of which 3 hours and 20 minutes were spent collecting data. One calibration exercise totaling 30 minutes occurred while surveying the blind grid.

3.4.3 Downtime Occasions

Occasions of downtime are grouped into five categories: equipment/data checks or equipment maintenance, equipment failure and repair, weather, demonstration site issues, or breaks/lunch. All downtime is included for the purposes of calculating labor costs (section 5) except for downtime due to demonstration site issues. Demonstration site issues, while noted in the daily log, are considered nonchargeable downtime for the purposes of calculating labor costs and are not discussed. Breaks and lunches are discussed in this section and billed to the total site survey area.

3.4.3.1 Equipment/data checks, maintenance

Equipment data checks and maintenance activities accounted for no site usage time. These activities included changing out batteries and performing routine data checks to ensure the data were being properly recorded/collected. Sky Research spent no additional time for breaks and lunches.

3.4.3.2 Equipment failure or repair. No time was needed to resolve equipment failures that occurred while surveying the blind grid.

3.4.3.3 Weather. No weather delays occurred during the survey.

3.4.4 Data Collection. Sky Research spent a total time of 2 hours and 15 minutes in the blind grid area, 1 hour and 25 minutes of which were spent collecting data.

3.4.5 Demobilization

The Sky Research survey crew went on to conduct a full demonstration of the site. Therefore, demobilization did not occur until 17 February 2006. On that day, it took the crew 1 hour and 45 minutes to break down and pack up their equipment.

3.5 PROCESSING TIME

Sky Research submitted the raw data from the demonstration activities on the last day of the demonstration, as required. The scoring submittal data were provided well after the required 30-day time frame.

3.6 DEMONSTRATOR'S FIELD PERSONNEL

Geophysicist: Craig Hyslop
Geophysicist: John Jacobsen
Geophysicist: Rob Mehl

3.7 DEMONSTRATOR'S FIELD SURVEYING METHOD

Sky Research surveyed the moguls in a linear fashion. The line spacing was 1 meter.

3.8 SUMMARY OF DAILY LOGS

Daily logs captured all field activities during this demonstration and are located in Appendix D. Activities pertinent to this specific demonstration are indicated in highlighted text.

<u>**SECTION 4. TECHNICAL PERFORMANCE RESULTS**</u>

4.1 ROC CURVES USING ALL ORDNANCE CATEGORIES

The probability of detection for the response stage (P_d^{res}) and the discrimination stage (P_d^{disc}) versus their respective probability of false positive are shown in Figure 2. Both probabilities plotted against their respective probability of background alarm are shown in Figure 3. Both figures use horizontal lines to illustrate the performance of the demonstrator at two demonstrator-specified points: at the system noise level for the response stage, representing the point below which targets are not considered detectable, and at the demonstrator's recommended threshold level for the discrimination stage, defining the subset of targets the demonstrator would recommend digging based on discrimination. Note that all points have been rounded to protect the ground truth.

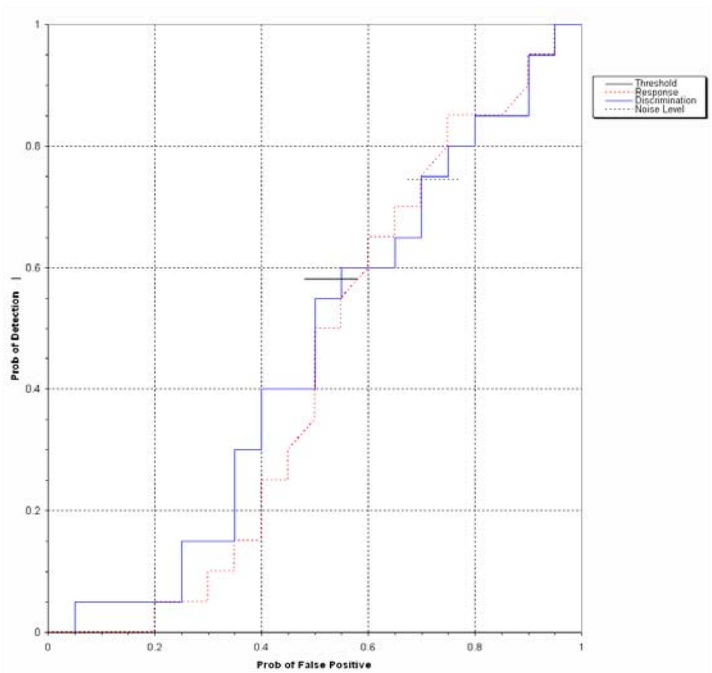

Figure 2. EM61 MKII/pushcart blind grid probability of detection for response and discrimination stages versus their respective probability of false positive over all ordnance categories combined.

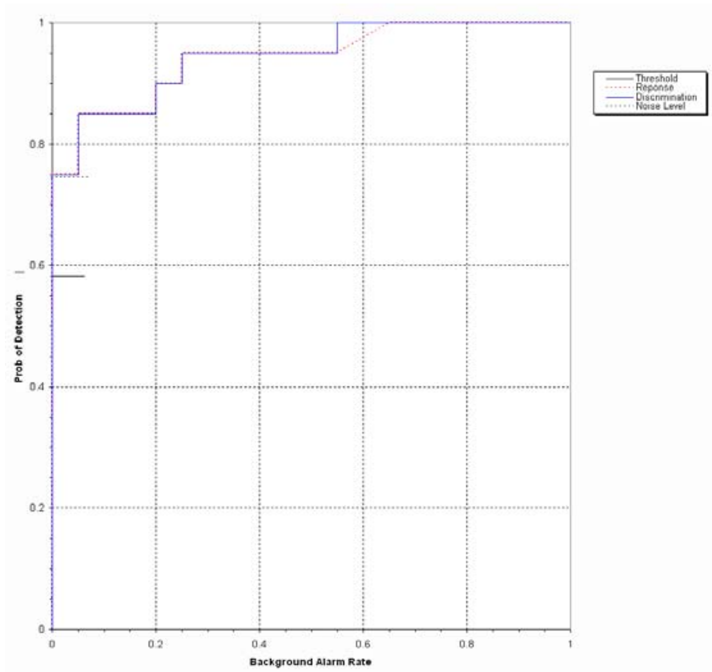

Figure 3. EM61 MKII/pushcart blind grid probability of detection for response and discrimination stages versus their respective probability of background alarm over all ordnance categories combined.

4.2 ROC CURVES USING ORDNANCE LARGER THAN 20 MM

The probability of detection for the response stage (P_d^{res}) and the discrimination stage (P_d^{disc}) versus their respective probability of false positive when only targets larger than 20 mm are scored are shown in Figure 4. Both probabilities plotted against their respective probability of background alarm are shown in Figure 5. Both figures use horizontal lines to illustrate the performance of the demonstrator at two demonstrator-specified points: at the system noise level for the response stage, representing the point below which targets are not considered detectable, and at the demonstrator's recommended threshold level for the discrimination stage, defining the subset of targets the demonstrator would recommend digging based on discrimination. Note that all points have been rounded to protect the ground truth.

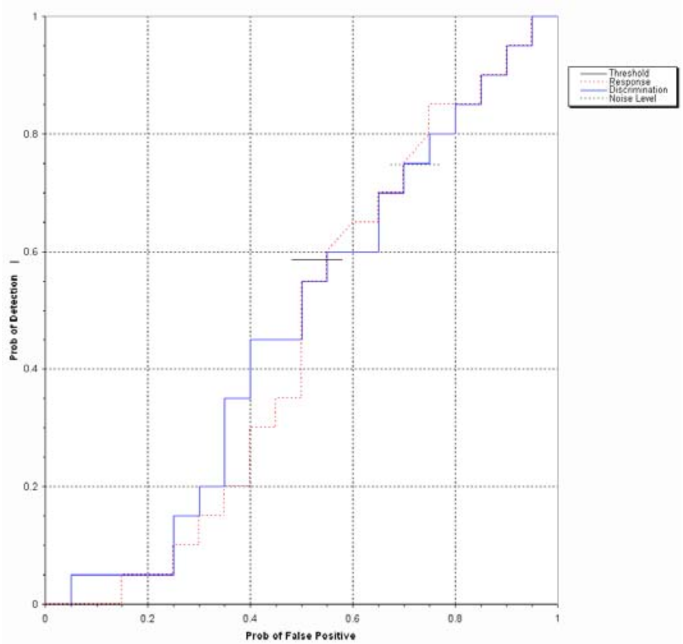

Figure 4. EM61 MKII/pushcart blind grid probability of detection for response and discrimination stages versus their respective probability of false positive for all ordnance larger than 20 mm.

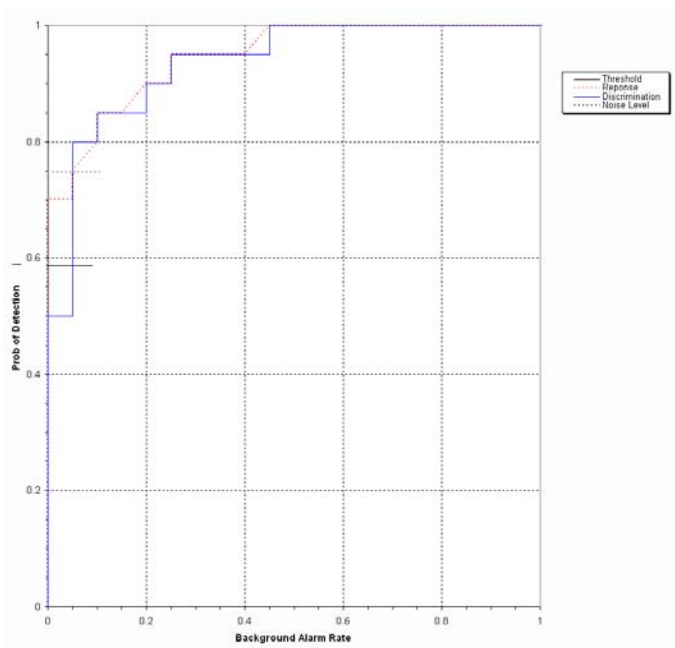

Figure 5. EM61 MKII/pushcart blind grid probability of detection for response and discrimination stages versus their respective probabilities of background alarm for all ordnance larger than 20 mm.

4.3 PERFORMANCE SUMMARIES

Results for the blind grid test broken out by size, depth, and nonstandard ordnance are presented in Table 5 (for cost results, see section 5). Results by size and depth include both standard and nonstandard ordnance. The results by size show how well the demonstrator did at detecting/discriminating ordnance of a certain caliber range (see app A for size definitions). The results are relative to the number of ordnance items emplaced. Depth is measured from the geometric center of anomalies.

The RESPONSE STAGE results are derived from the list of anomalies above the demonstrator-provided noise level. The results for the DISCRIMINATION STAGE are derived from the demonstrator's recommended threshold for optimizing UXO field cleanup by minimizing false digs and maximizing ordnance recovery. The lower 90 percent confidence limit on probability of detection and P_{fp} was calculated assuming that the number of detections and false positives are binomially distributed random variables. All results in Table 5 have been rounded to protect the ground truth. However, lower confidence limits were calculated using actual results.

TABLE 5. SUMMARY OF BLIND GRID RESULTS FOR THE EM61 MKII/PUSHCART

Metric	Overall	Standard	Nonstandard	By Size			By Depth, m		
				Small	Medium	Large	< 0.3	0.3 to <1	>= 1
RESPONSE STAGE									
P_d	0.75	0.80	0.65	0.80	0.65	0.90	0.95	0.65	0.45
P_d Low 90% Conf	0.67	0.74	0.51	0.69	0.51	0.66	0.89	0.54	0.26
P_d Upper 90% Conf	0.81	0.89	0.74	0.87	0.75	0.99	1.00	0.76	0.62
P_{fp}	0.70	-	-	-	-	-	0.80	0.70	0.65
P_{fp} Low 90% Conf	0.66	-	-	-	-	-	0.68	0.58	0.33
P_d Upper 90% Conf	0.78	-	-	-	-	-	0.87	0.77	0.91
P_{ba}	0.00	-	-	-	-	-	-	-	-
DISCRIMINATION STAGE									
P_d	0.60	0.65	0.45	0.65	0.50	0.60	0.85	0.50	0.20
P_d Low 90% Conf	0.51	0.57	0.34	0.54	0.36	0.35	0.75	0.37	0.07
P_d Upper 90% Conf	0.65	0.75	0.58	0.75	0.61	0.81	0.93	0.61	0.37
P_{fp}	0.55	-	-	-	-	-	0.55	0.55	0.35
P_{fp} Low 90% Conf	0.46	-	-	-	-	-	0.44	0.44	0.09
P_d Upper 90% Conf	0.60	-	-	-	-	-	0.65	0.64	0.67
P_{ba}	0.00	-	-	-	-	-	-	-	-

Response Stage Noise Level: 2.68.
Recommended Discrimination Stage Threshold: 295.5.

Note: The recommended discrimination stage threshold values are provided by the demonstrator.

4.4 EFFICIENCY, REJECTION RATES, AND TYPE CLASSIFICATION

Efficiency and rejection rates are calculated to quantify the discrimination ability at specific points of interest on the ROC curve: (1) at the point where no decrease in P_d is suffered (i.e., the efficiency is by definition equal to one) and (2) at the operator selected threshold. These values are reported in Table 6.

TABLE 6. EFFICIENCY AND REJECTION RATES

	Efficiency (E)	False Positive Rejection Rate	Background Alarm Rejection Rate
At Operating Point	0.78	0.27	0.40
With No Loss of P_d	1.05	-0.04	-0.2

At the demonstrator's recommended setting, the ordnance items that were detected and correctly discriminated were further scored on whether their correct type could be identified (table 7). Correct type examples include 20-mm projectile, 105-mm HEAT Projectile, and 2.75-inch Rocket. A list of the standard type declaration required for each ordnance item was provided to demonstrators prior to testing. For example, the standard types for the three example items are 20mmP, 105H, and 2.75in, respectively.

TABLE 7. CORRECT TYPE CLASSIFICATION OF TARGETS CORRECTLY DISCRIMINATED AS UXO

Size	Percentage Correct
Small	0.0
Medium	0.0
Large	0.0
Overall	0.0

Note: The demonstrator did not attempt to provide type classification.

4.5 LOCATION ACCURACY

The mean location error and standard deviations appear in Table 8. These calculations are based on average missed depth for ordnance correctly identified in the discrimination stage. Depths are measured from the closest point of the ordnance to the surface. For the blind grid, only depth errors are calculated because (X, Y) positions are known to be the centers of each grid square.

TABLE 8. MEAN LOCATION ERROR AND STANDARD DEVIATION (M)

	Mean	Standard Deviation
Depth	-0.84	0.51

SECTION 5. ON-SITE LABOR COSTS

A standardized estimate for labor costs associated with this effort was calculated as follows: the first person at the test site was designated supervisor, the second person was designated data analyst, and the third and following personnel were considered field support. Standardized hourly labor rates were charged by title: supervisor at $95.00/hour, data analyst at $57.00/hour, and field support at $28.50/hour.

Government representatives monitored on-site activity. All on-site activities were grouped into one of ten categories: initial setup/mobilization, daily setup/stop, calibration, data collection, downtime due to break/lunch, downtime due to equipment failure, downtime due to equipment/data checks or maintenance, downtime due to weather, downtime due to demonstration site issue, or demobilization. See Appendix D for the daily activity log. See section 3.4 for a summary of field activities.

The standardized cost estimate associated with the labor needed to perform the field activities is presented in Table 9. Note that calibration time includes time spent in the calibration lanes as well as field calibrations. Site survey time includes daily setup/stop time, collecting data, breaks/lunch, downtime due to equipment/data checks or maintenance, downtime due to failure, and downtime due to weather.

TABLE 9. ON-SITE LABOR COSTS

	No. People	Hourly Wage	Hours	Cost
Initial setup				
Supervisor	1	$95.00	12.25	$1163.75
Data analyst	1	57.00	12.25	698.25
Field support	1	28.50	12.25	349.13
Subtotal				**$2211.13**
Calibration				
Supervisor	1	$95.00	12.16	$1155.20
Data analyst	1	57.00	12.16	693.12
Field support	1	28.50	12.16	346.56
Subtotal				**$2194.88**
Site survey				
Supervisor	1	$95.00	2.25	$213.75
Data analyst	1	57.00	2.25	128.25
Field support	1	28.50	2.25	64.13
Subtotal				**$406.13**

See notes at end of table.

TABLE 9 (CONT'D)

	No. People	Hourly Wage	Hours	Cost
Demobilization				
Supervisor	1	$95.00	1.75	$166.25
Data analyst	1	57.00	1.75	99.75
Field support	1	28.50	1.75	49.88
Subtotal				$315.88
Total				**$5128.02**

Notes: Calibration time includes time spent in the calibration lanes as well as calibration before each data run.

Site survey time includes daily setup/stop time, data collection, breaks/lunch, and downtime due to system maintenance, failure, and weather.

SECTION 6. COMPARISON OF RESULTS TO DATE

No comparisons to date.

SECTION 7. APPENDIXES

APPENDIX A. TERMS AND DEFINITIONS

GENERAL DEFINITIONS

Anomaly: Location of a system response deemed to warrant further investigation by the demonstrator for consideration as an emplaced ordnance item.

Detection: An anomaly location that is within R_{halo} of an emplaced ordnance item.

Munitions and Explosives Of Concern (MEC): Specific categories of military munitions that may pose unique explosive safety risks, including UXO as defined in 10 USC 101(e)(5), DMM as defined in 10 USC 2710(e)(2) and/or munitions constituents (e.g. TNT, RDX) as defined in 10 USC 2710(e)(3) that are present in high enough concentrations to pose an explosive hazard.

Emplaced Ordnance: An ordnance item buried by the government at a specified location in the test site.

Emplaced Clutter: A clutter item (i.e., non-ordnance item) buried by the government at a specified location in the test site.

R_{halo}: A pre-determined radius about the periphery of an emplaced item (clutter or ordnance) within which a location identified by the demonstrator as being of interest is considered to be a response from that item. If multiple declarations lie within R_{halo} of any item (clutter or ordnance), the declaration with the highest signal output within the R_{halo} will be utilized. For the purpose of this program, a circular halo 0.5 meters in radius will be placed around the center of the object for all clutter and ordnance items less than 0.6 meters in length. When ordnance items are longer than 0.6 meters, the halo becomes an ellipse where the minor axis remains 1 meter and the major axis is equal to the length of the ordnance plus 1 meter.

Small Ordnance: Caliber of ordnance less than or equal to 40 mm (includes 20-mm projectile, 40-mm projectile, submunitions BLU-26, BLU-63, and M42).

Medium Ordnance: Caliber of ordnance greater than 40 mm and less than or equal to 81 mm (includes 57-mm projectile, 60-mm mortar, 2.75 in. Rocket, MK118 Rockeye, 81-mm mortar).

Large Ordnance: Caliber of ordnance greater than 81 mm (includes 105-mm HEAT, 105-mm projectile, 155-mm projectile, 500-pound bomb).

Shallow: Items buried less than 0.3 meter below ground surface.

Medium: Items buried greater than or equal to 0.3 meter and less than 1 meter below ground surface.

Deep: Items buried greater than or equal to 1 meter below ground surface.

Response Stage Noise Level: The level that represents the point below which anomalies are not considered detectable. Demonstrators are required to provide the recommended noise level for the blind grid test area.

Discrimination Stage Threshold: The demonstrator selected threshold level that they believe provides optimum performance of the system by retaining all detectable ordnance and rejecting the maximum amount of clutter. This level defines the subset of anomalies the demonstrator would recommend digging based on discrimination.

Binomially Distributed Random Variable: A random variable of the type which has only two possible outcomes, say success and failure, is repeated for n independent trials with the probability p of success and the probability 1-p of failure being the same for each trial. The number of successes x observed in the n trials is an estimate of p and is considered to be a binomially distributed random variable.

RESPONSE AND DISCRIMINATION STAGE DATA

The scoring of the demonstrator's performance is conducted in two stages. These two stages are termed the RESPONSE STAGE and DISCRIMINATION STAGE. For both stages, the probability of detection (P_d) and the false alarms are reported as receiver operating characteristic (ROC) curves. False alarms are divided into those anomalies that correspond to emplaced clutter items, measuring the probability of false positive (P_{fp}) and those that do not correspond to any known item, termed background alarms.

The RESPONSE STAGE scoring evaluates the ability of the system to detect emplaced targets without regard to ability to discriminate ordnance from other anomalies. For the RESPONSE STAGE, the demonstrator provides the scoring committee with the location and signal strength of all anomalies that the demonstrator has deemed sufficient to warrant further investigation and/or processing as potential emplaced ordnance items. This list is generated with minimal processing (e.g., this list will include all signals above the system noise threshold). As such, it represents the most inclusive list of anomalies.

The DISCRIMINATION STAGE evaluates the demonstrator's ability to correctly identify ordnance as such, and to reject clutter. For the same locations as in the RESPONSE STAGE anomaly list, the DISCRIMINATION STAGE list contains the output of the algorithms applied in the discrimination-stage processing. This list is prioritized based on the demonstrator's determination that an anomaly location is likely to contain ordnance. Thus, higher output values are indicative of higher confidence that an ordnance item is present at the specified location. For electronic signal processing, priority ranking is based on algorithm output. For other systems, priority ranking is based on human judgment. The demonstrator also selects the threshold that the demonstrator believes will provide "optimum" system performance, (i.e., that retains all the detected ordnance and rejects the maximum amount of clutter).

Note: The two lists provided by the demonstrator contain identical numbers of potential target locations. They differ only in the priority ranking of the declarations.

RESPONSE STAGE DEFINITIONS

Response Stage Probability of Detection (P_d^{res}): P_d^{res} = (No. of response-stage detections)/(No. of emplaced ordnance in the test site).

Response Stage False Positive (fp^{res}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Response Stage Probability of False Positive (P_{fp}^{res}): P_{fp}^{res} = (No. of response-stage false positives)/(No. of emplaced clutter items).

Response Stage Background Alarm (ba^{res}): An anomaly in a blind grid cell that contains neither emplaced ordnance nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced ordnance or emplaced clutter item.

Response Stage Probability of Background Alarm (P_{ba}^{res}): Blind Grid only: P_{ba}^{res} = (No. of response-stage background alarms)/(No. of empty grid locations).

Response Stage Background Alarm Rate (BAR^{res}): Open Field only: BAR^{res} = (No. of response-stage background alarms)/(arbitrary constant).

Note that the quantities P_d^{res}, P_{fp}^{res}, P_{ba}^{res}, and BAR^{res} are functions of t^{res}, the threshold applied to the response-stage signal strength. These quantities can therefore be written as $P_d^{res}(t^{res})$, $P_{fp}^{res}(t^{res})$, $P_{ba}^{res}(t^{res})$, and $BAR^{res}(t^{res})$.

DISCRIMINATION STAGE DEFINITIONS

Discrimination: The application of a signal processing algorithm or human judgment to response-stage data that discriminates ordnance from clutter. Discrimination should identify anomalies that the demonstrator has high confidence correspond to ordnance, as well as those that the demonstrator has high confidence correspond to non-ordnance or background returns. The former should be ranked with highest priority and the latter with lowest.

Discrimination Stage Probability of Detection (P_d^{disc}): P_d^{disc} = (No. of discrimination-stage detections)/(No. of emplaced ordnance in the test site).

Discrimination Stage False Positive (fp^{disc}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Discrimination Stage Probability of False Positive (P_{fp}^{disc}): P_{fp}^{disc} = (No. of discrimination stage false positives)/(No. of emplaced clutter items).

Discrimination Stage Background Alarm (ba^{disc}): An anomaly in a blind grid cell that contains neither emplaced ordnance nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced ordnance or emplaced clutter item.

Discrimination Stage Probability of Background Alarm (P_{ba}^{disc}): P_{ba}^{disc} = (No. of discrimination-stage background alarms)/(No. of empty grid locations).

Discrimination Stage Background Alarm Rate (BAR^{disc}): BAR^{disc} = (No. of discrimination-stage background alarms)/(arbitrary constant).

Note that the quantities P_d^{disc}, P_{fp}^{disc}, P_{ba}^{disc}, and BAR^{disc} are functions of t^{disc}, the threshold applied to the discrimination-stage signal strength. These quantities can therefore be written as $P_d^{disc}(t^{disc})$, $P_{fp}^{disc}(t^{disc})$, $P_{ba}^{disc}(t^{disc})$, and $BAR^{disc}(t^{disc})$.

RECEIVER-OPERATING CHARACERISTIC (ROC) CURVES

ROC curves at both the response and discrimination stages can be constructed based on the above definitions. The ROC curves plot the relationship between P_d versus P_{fp} and P_d versus BAR or P_{ba} as the threshold applied to the signal strength is varied from its minimum (t_{min}) to its maximum (t_{max}) value.[1] Figure A-1 shows how P_d versus P_{fp} and P_d versus BAR are combined into ROC curves. Note that the "res" and "disc" superscripts have been suppressed from all the variables for clarity.

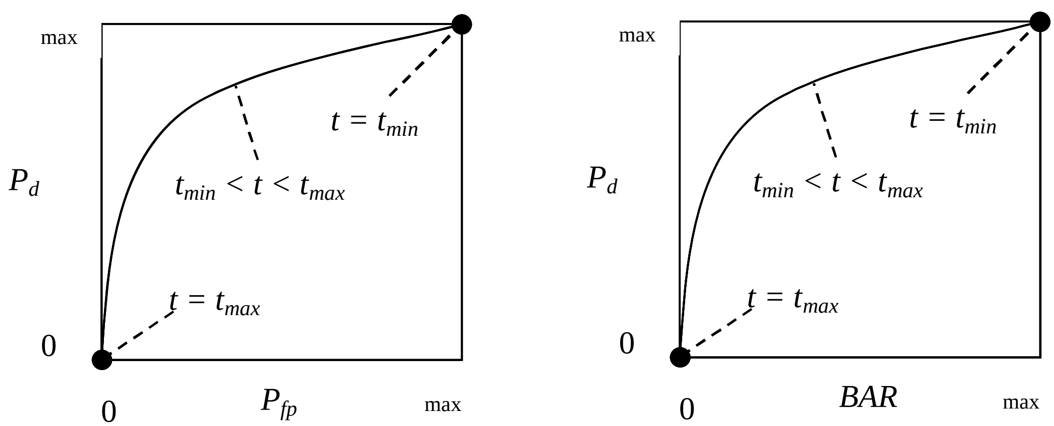

Figure A-1. ROC curves for open field testing. Each curve applies to both the response and discrimination stages.

[1]Strictly speaking, ROC curves plot the P_d versus P_{ba} over a pre-determined and fixed number of detection opportunities (some of the opportunities are located over ordnance and others are located over clutter or blank spots). In an open field scenario, each system suppresses its signal strength reports until some bare-minimum signal response is received by the system. Consequently, the open field ROC curves do not have information from low signal-output locations, and, furthermore, different contractors report their signals over a different set of locations on the ground. These ROC curves are thus not true to the strict definition of ROC curves as defined in textbooks on detection theory. Note, however, that the ROC curves obtained in the blind grid test sites are true ROC curves.

METRICS TO CHARACTERIZE THE DISCRIMINATION STAGE

The demonstrator is also scored on efficiency and rejection ratio, which measure the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of ordnance detections from the anomaly list, while rejecting the maximum number of anomalies arising from non-ordnance items. The efficiency measures the amount of detected ordnance retained by the discrimination, while the rejection ratio measures the fraction of false alarms rejected. Both measures are defined relative to the entire response list, i.e., the maximum ordnance detectable by the sensor and its accompanying false positive rate or background alarm rate.

Efficiency (E): $E = P_d^{disc}(t^{disc})/P_d^{res}(t_{min}^{res})$; Measures (at a threshold of interest), the degree to which the maximum theoretical detection performance of the sensor system (as determined by the response stage t_{min}) is preserved after application of discrimination techniques. Efficiency is a number between 0 and 1. An efficiency of 1 implies that all of the ordnance initially detected in the response stage was retained at the specified threshold in the discrimination stage, t^{disc}.

False Positive Rejection Rate (R_{fp}): $R_{fp} = 1 - [P_{fp}^{disc}(t^{disc})/P_{fp}^{res}(t_{min}^{res})]$; Measures (at a threshold of interest), the degree to which the sensor system's false positive performance is improved over the maximum false positive performance (as determined by the response stage tmin). The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all emplaced clutter initially detected in the response stage were correctly rejected at the specified threshold in the discrimination stage.

Background Alarm Rejection Rate (R_{ba}):

Blind grid: $R_{ba} = 1 - [P_{ba}^{disc}(t^{disc})/P_{ba}^{res}(t_{min}^{res})]$.
Open field: $R_{ba} = 1 - [BAR^{disc}(t^{disc})/BAR^{res}(t_{min}^{res})])$.

Measures the degree to which the discrimination stage correctly rejects background alarms initially detected in the response stage. The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all background alarms initially detected in the response stage were rejected at the specified threshold in the discrimination stage.

CHI-SQUARE COMPARISON EXPLANATION:

The Chi-square test for differences in probabilities (or 2 x 2 contingency table) is used to analyze two samples drawn from two different populations to see if both populations have the same or different proportions of elements in a certain category. More specifically, two random samples are drawn, one from each population, to test the null hypothesis that the probability of event A (some specified event) is the same for both populations.

A 2 x 2 contingency table is used in the Standardized UXO Technology Demonstration Site Program to determine if there is reason to believe that the proportion of ordnance correctly detected/discriminated by demonstrator X’s system is significantly degraded by the more challenging terrain feature introduced. The test statistic of the 2 x 2 contingency table is the

Chi-square distribution with one degree of freedom. Since an association between the more challenging terrain feature and relatively degraded performance is sought, a one-sided test is performed. A significance level of 0.05 is chosen which sets a critical decision limit of 2.71 from the Chi-square distribution with one degree of freedom. It is a critical decision limit because if the test statistic calculated from the data exceeds this value, the two proportions tested will be considered significantly different. If the test statistic calculated from the data is less than this value, the two proportions tested will be considered not significantly different.

An exception must be applied when either a 0 or 100 percent success rate occurs in the sample data. The Chi-square test cannot be used in these instances. Instead, Fischer's test is used and the critical decision limit for one-sided tests is the chosen significance level, which in this case is 0.05. With Fischer's test, if the test statistic is less than the critical value, the proportions are considered to be significantly different.

Standardized UXO Technology Demonstration Site examples, where blind grid results are compared to those from the open field and open field results are compared to those from one of the scenarios, follow. It should be noted that a significant result does not prove a cause and effect relationship exists between the two populations of interest; however, it does serve as a tool to indicate that one data set has experienced a degradation in system performance at a large enough level than can be accounted for merely by chance or random variation. Note also that a result that is not significant indicates that there is not enough evidence to declare that anything more than chance or random variation within the same population is at work between the two data sets being compared.

Demonstrator X achieves the following overall results after surveying each of the three progressively more difficult areas using the same system (results indicate the number of ordnance detected divided by the number of ordnance emplaced):

	Blind grid	Open field	Moguls
P_d^{res}	100/100 = 1.0	8/10 = .80	20/33 = .61
P_d^{disc}	80/100 = 0.80	6/10 = .60	8/33 = .24

P_d^{res}: BLIND GRID versus OPEN FIELD. Using the example data above to compare probabilities of detection in the response stage, all 100 ordnance out of 100 emplaced ordnance items were detected in the blind grid while 8 ordnance out of 10 emplaced were detected in the open field. Fischer's test must be used since a 100 percent success rate occurs in the data. Fischer's test uses the four input values to calculate a test statistic of 0.0075 that is compared against the critical value of 0.05. Since the test statistic is less than the critical value, the smaller response stage detection rate (0.80) is considered to be significantly less at the 0.05 level of significance. While a significant result does not prove a cause and effect relationship exists between the change in survey area and degradation in performance, it does indicate that the detection ability of demonstrator X's system seems to have been degraded in the open field relative to results from the blind grid using the same system.

P_d^{disc}: BLIND GRID versus OPEN FIELD. Using the example data above to compare probabilities of detection in the discrimination stage, 80 out of 100 emplaced ordnance items were correctly discriminated as ordnance in blind grid testing while 6 ordnance out of 10 emplaced were correctly discriminated as such in open field-testing. Those four values are used to calculate a test statistic of 1.12. Since the test statistic is less than the critical value of 2.71, the two discrimination stage detection rates are considered to be not significantly different at the 0.05 level of significance.

P_d^{res}: OPEN FIELD versus MOGULS. Using the example data above to compare probabilities of detection in the response stage, 8 out of 10 and 20 out of 33 are used to calculate a test statistic of 0.56. Since the test statistic is less than the critical value of 2.71, the two response stage detection rates are considered to be not significantly different at the 0.05 level of significance.

P_d^{disc}: OPEN FIELD versus MOGULS. Using the example data above to compare probabilities of detection in the discrimination stage, 6 out of 10 and 8 out of 33 are used to calculate a test statistic of 2.98. Since the test statistic is greater than the critical value of 2.71, the smaller discrimination stage detection rate is considered to be significantly less at the 0.05 level of significance. While a significant result does not prove a cause and effect relationship exists between the change in survey area and degradation in performance, it does indicate that the ability of demonstrator X to correctly discriminate seems to have been degraded by the mogul terrain relative to results from the flat open field using the same system.

APPENDIX B. DAILY WEATHER LOGS

Date, 06	Time, EST	Average Temperature, ^oF	Total Precipitation, in.
30 Jan	0700	33.5	0.01
30 Jan	0800	34.4	0.00
30 Jan	0900	37.3	0.00
30 Jan	1000	40.9	0.00
30 Jan	1100	43.9	0.00
30 Jan	1200	47.2	0.00
30 Jan	1300	48.9	0.00
30 Jan	1400	52.5	0.00
30 Jan	1500	56.2	0.00
30 Jan	1600	57.8	0.00
30 Jan	1700	56.3	0.00
31 Jan	0700	44.5	0.00
31 Jan	0800	44.2	0.00
31 Jan	0900	43.8	0.00
31 Jan	1000	44.0	0.00
31 Jan	1100	45.7	0.00
31 Jan	1200	45.3	0.00
31 Jan	1300	46.0	0.00
31 Jan	1400	46.7	0.00
31 Jan	1500	46.4	0.00
31 Jan	1600	45.5	0.00
31 Jan	1700	45.2	0.00
1 Feb	0700	38.4	0.00
1 Feb	0800	38.5	0.00
1 Feb	0900	38.9	0.00
1 Feb	1000	39.7	0.00
1 Feb	1100	40.4	0.00
1 Feb	1200	41.0	0.00
1 Feb	1300	42.1	0.00
1 Feb	1400	43.2	0.00
1 Feb	1500	44.6	0.00
1 Feb	1600	43.6	0.00
1 Feb	1700	41.9	0.00

Date, 06	Time, EST	Average Temperature, ^oF	Total Precipitation, in.
2 Feb	0700	30.0	0.00
2 Feb	0800	31.5	0.00
2 Feb	0900	35.9	0.00
2 Feb	1000	42.1	0.00
2 Feb	1100	45.4	0.00
2 Feb	1200	48.1	0.00
2 Feb	1300	50.5	0.00
2 Feb	1400	52.7	0.00
2 Feb	1500	54.3	0.00
2 Feb	1600	54.0	0.00
2 Feb	1700	53.5	0.00
3 Feb	0700	58.3	0.00
3 Feb	0800	58.0	0.03
3 Feb	0900	54.3	0.01
3 Feb	1000	54.3	0.00
3 Feb	1100	56.3	0.00
3 Feb	1200	59.3	0.00
3 Feb	1300	60.8	0.00
3 Feb	1400	61.6	0.00
3 Feb	1500	62.1	0.00
3 Feb	1600	61.3	0.00
3 Feb	1700	62.0	0.00
4 Feb	0700	44.7	0.00
4 Feb	0800	45.6	0.00
4 Feb	0900	46.9	0.00
4 Feb	1000	48.1	0.00
4 Feb	1100	49.3	0.00
4 Feb	1200	48.0	0.01
4 Feb	1300	47.4	0.02
4 Feb	1400	48.1	0.14
4 Feb	1500	47.8	0.32
4 Feb	1600	48.0	0.18
4 Feb	1700	48.3	0.00
5 Feb	0700	38.0	0.00
5 Feb	0800	37.0	0.00
5 Feb	0900	39.7	0.00
5 Feb	1000	42.5	0.00
5 Feb	1100	43.0	0.00
5 Feb	1200	43.4	0.00
5 Feb	1300	44.3	0.00
5 Feb	1400	43.9	0.00
5 Feb	1500	44.1	0.00
5 Feb	1600	43.6	0.00
5 Feb	1700	42.8	0.00

Date, 06	Time, EST	Average Temperature, ^oF	Total Precipitation, in.
6 Feb	0700	33.0	0.00
6 Feb	0800	33.9	0.00
6 Feb	0900	35.2	0.00
6 Feb	1000	36.4	0.00
6 Feb	1100	37.2	0.00
6 Feb	1200	38.7	0.00
6 Feb	1300	40.2	0.00
6 Feb	1400	41.5	0.00
6 Feb	1500	43.2	0.00
6 Feb	1600	44.4	0.00
6 Feb	1700	43.9	0.00
7 Feb	0700	30.9	0.00
7 Feb	0800	30.2	0.00
7 Feb	0900	33.8	0.00
7 Feb	1000	35.4	0.00
7 Feb	1100	37.0	0.00
7 Feb	1200	38.5	0.00
7 Feb	1300	39.8	0.00
7 Feb	1400	41.0	0.00
7 Feb	1500	41.6	0.00
7 Feb	1600	41.6	0.00
7 Feb	1700	40.4	0.00
8 Feb	0700	25.9	0.00
8 Feb	0800	25.3	0.00
8 Feb	0900	29.9	0.00
8 Feb	1000	33.0	0.00
8 Feb	1100	35.0	0.00
8 Feb	1200	34.9	0.00
8 Feb	1300	36.0	0.00
8 Feb	1400	35.4	0.00
8 Feb	1500	36.3	0.00
8 Feb	1600	36.3	0.00
8 Feb	1700	35.3	0.00
9 Feb	0700	26.4	0.00
9 Feb	0800	27.1	0.00
9 Feb	0900	29.1	0.00
9 Feb	1000	30.5	0.00
9 Feb	1100	32.1	0.00
9 Feb	1200	33.5	0.00
9 Feb	1300	35.1	0.00
9 Feb	1400	36.2	0.00
9 Feb	1500	37.0	0.00
9 Feb	1600	37.5	0.00
9 Feb	1700	36.7	0.00

Date, 06	Time, EST	Average Temperature, °F	Total Precipitation, in.
10 Feb	0700	28.3	0.00
10 Feb	0800	28.8	0.00
10 Feb	0900	30.6	0.00
10 Feb	1000	33.1	0.00
10 Feb	1100	35.8	0.00
10 Feb	1200	37.5	0.00
10 Feb	1300	38.0	0.00
10 Feb	1400	38.1	0.00
10 Feb	1500	38.8	0.00
10 Feb	1600	39.4	0.00
10 Feb	1700	39.1	0.00
11 Feb	0700	33.4	0.00
11 Feb	0800	33.7	0.00
11 Feb	0900	35.1	0.00
11 Feb	1000	36.7	0.00
11 Feb	1100	38.7	0.00
11 Feb	1200	39.8	0.00
11 Feb	1300	40.3	0.00
11 Feb	1400	38.1	0.00
11 Feb	1500	35.4	0.00
11 Feb	1600	34.1	0.00
11 Feb	1700	33.1	0.01
12 Feb	0700	26.7	0.00
12 Feb	0800	26.4	0.00
12 Feb	0900	26.5	0.00
12 Feb	1000	27.1	0.00
12 Feb	1100	29.1	0.00
12 Feb	1200	29.8	0.01
12 Feb	1300	30.5	0.02
12 Feb	1400	31.7	0.02
12 Feb	1500	33.4	0.03
12 Feb	1600	34.3	0.02
12 Feb	1700	33.9	0.01
13 Feb	0700	17.3	0.00
13 Feb	0800	17.9	0.00
13 Feb	0900	22.5	0.00
13 Feb	1000	26.8	0.00
13 Feb	1100	30.9	0.00
13 Feb	1200	33.6	0.01
13 Feb	1300	35.4	0.01
13 Feb	1400	36.5	0.04
13 Feb	1500	36.2	0.02
13 Feb	1600	35.6	0.01
13 Feb	1700	35.6	0.00

Date, 06	Time, EST	Average Temperature, °F	Total Precipitation, in.
14 Feb	0700	17.9	0.00
14 Feb	0800	20.2	0.00
14 Feb	0900	26.8	0.00
14 Feb	1000	31.9	0.00
14 Feb	1100	37.0	0.01
14 Feb	1200	39.2	0.03
14 Feb	1300	40.5	0.03
14 Feb	1400	41.1	0.02
14 Feb	1500	41.3	0.01
14 Feb	1600	41.4	0.00
14 Feb	1700	41.4	0.00
15 Feb	0700	23.5	0.00
15 Feb	0800	24.7	0.00
15 Feb	0900	33.6	0.00
15 Feb	1000	40.0	0.00
15 Feb	1100	49.3	0.00
15 Feb	1200	48.6	0.00
15 Feb	1300	48.1	0.00
15 Feb	1400	48.9	0.00
15 Feb	1500	50.5	0.00
15 Feb	1600	50.5	0.17
15 Feb	1700	50.6	0.00
16 Feb	0700	28.9	0.00
16 Feb	0800	29.6	0.00
16 Feb	0900	37.8	0.00
16 Feb	1000	44.5	0.00
16 Feb	1100	49.8	0.00
16 Feb	1200	51.4	0.00
16 Feb	1300	52.7	0.00
16 Feb	1400	54.9	0.00
16 Feb	1500	56.9	0.00
16 Feb	1600	60.7	0.00
16 Feb	1700	56.4	0.00
17 Feb	0700	54.5	0.00
17 Feb	0800	54.4	0.01
17 Feb	0900	52.3	0.00
17 Feb	1000	55.1	0.00
17 Feb	1100	58.7	0.00
17 Feb	1200	57.2	0.00
17 Feb	1300	53.3	0.00
17 Feb	1400	51.7	0.00
17 Feb	1500	50.5	0.00
17 Feb	1600	49.4	0.00
17 Feb	1700	48.3	0.00

APPENDIX C. SOIL MOISTURE

Date: 30 Jan 06			
Times: 1100 through 1600			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Calibration lanes	0 to 6	3.4	3.3
	6 to 12	16.8	16.9
	12 to 24	24.8	24.5
	24 to 36	29.2	29.1
	36 to 48	31.7	31.6
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

Date: 31 Jan 06			
Times: 0900 through 1400			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Calibration lanes	0 to 6	3.2	3.2
	6 to 12	16.7	16.6
	12 to 24	24.6	24.7
	24 to 36	29.5	29.7
	36 to 48	31.4	31.3
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

Date: 1 Feb 06			
Times: 0900 through 1400			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Calibration lanes	0 to 6	3.2	3.2
	6 to 12	16.7	16.6
	12 to 24	24.6	24.7
	24 to 36	29.5	29.7
	36 to 48	31.4	31.3
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

Date: 2 Feb 06			
Times: 0900 through 1500			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6	5.8	5.7
	6 to 12	12.9	13.1
	12 to 24	16.4	16.5
	24 to 36	21.9	21.8
	36 to 48	30.2	30.7

Date: 3 Feb 06			
Times: 1000 through 1400			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Calibration lanes	0 to 6	2.8	2.7
	6 to 12	16.5	16.6
	12 to 24	24.2	24.4
	24 to 36	29.8	29.6
	36 to 48	31.2	31.4
Blind grid/moguls	0 to 6	5.9	5.8
	6 to 12	13.8	13.7
	12 to 24	16.9	16.7
	24 to 36	21.4	21.5
	36 to 48	30.5	30.5

Date: 6 Feb 06			
Times: 0900 through 1400			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6	4.9	4.7
	6 to 12	8.8	8.7
	12 to 24	16.8	16.9
	24 to 36	4.8	4.7
	36 to 48	4.6	4.5
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6	5.8	5.7
	6 to 12	6.9	6.4
	12 to 24	4.7	4.6
	24 to 36	12.5	12.6
	36 to 48	22.9	22.7
Calibration lanes	0 to 6	2.9	2.8
	6 to 12	16.2	16.1
	12 to 24	24.1	24.3
	24 to 36	29.5	29.4
	36 to 48	31.6	31.7
Blind grid/moguls	0 to 6	5.6	5.5
	6 to 12	13.9	13.7
	12 to 24	16.4	16.6
	24 to 36	21.2	21.3
	36 to 48	30.7	30.8

Date: 7 Feb 06			
Times: 1000 through 1700			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6	4.6	4.6
	6 to 12	8.9	8.8
	12 to 24	16.6	16.9
	24 to 36	4.5	4.4
	36 to 48	4.3	4.2
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6	5.9	5.8
	6 to 12	6.7	6.6
	12 to 24	4.5	4.4
	24 to 36	12.8	12.7
	36 to 48	22.5	22.4
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

Date: 8 Feb 06			
Times: 1000 through 1330			
Probe location	**Layer, inches**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6	4.4	4.3
	6 to 12	8.6	8.7
	12 to 24	16.5	16.2
	24 to 36	4.7	4.5
	36 to 48	4.1	4.0
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6	5.6	5.5
	6 to 12	6.9	6.4
	12 to 24	4.7	4.6
	24 to 36	12.9	12.5
	36 to 48	22.2	22.3
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6	5.9	5.8
	6 to 12	13.5	13.5
	12 to 24	16.5	16.6
	24 to 36	21.0	20.8
	36 to 48	30.5	30.4

Date: 9 Feb 06			
Times: 0900 through 1530			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Wooded area	0 to 6	8.7	8.6
	6 to 12	11.2	11.4
	12 to 24	13.9	13.8
	24 to 36	19.5	19.7
	36 to 48	19.6	20.1
Open area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6	5.7	5.6
	6 to 12	13.1	13.3
	12 to 24	16.4	16.3
	24 to 36	20.5	20.4
	36 to 48	30.3	30.4

Date: 10 Feb 06			
Times: 1000 through 1645			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Wooded area	0 to 6	8.4	8.3
	6 to 12	11.8	11.7
	12 to 24	13.4	13.6
	24 to 36	19.4	19.5
	36 to 48	19.7	19.9
Open area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

Date: 11 Feb 06			
Times: 0800 through 1400			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6	5.9	5.8
	6 to 12	8.4	8.2
	12 to 24	16.4	16.3
	24 to 36	4.9	4.6
	36 to 48	4.2	4.1
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6	5.4	5.7
	6 to 12	6.8	6.5
	12 to 24	4.9	4.7
	24 to 36	12.7	12.6
	36 to 48	22.4	22.4
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

Date: 13 Feb 06			
Times: 1000 through 1500			
Probe location	**Layer, inches**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6	7.2	7.5
	6 to 12	10.5	10.9
	12 to 24	16.9	17.2
	24 to 36	5.8	6.2
	36 to 48	8.4	8.3
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6	8.1	8.4
	6 to 12	7.4	7.2
	12 to 24	6.8	6.9
	24 to 36	13.5	13.8
	36 to 48	21.8	21.9
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

Date: 14 Feb 06			
Times: 1000 through 1530			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Calibration lanes	0 to 6	6.8	6.8
	6 to 12	17.8	17.9
	12 to 24	26.4	26.6
	24 to 36	29.8	29.9
	36 to 48	31.1	31.4
Blind grid/moguls	0 to 6	7.8	7.7
	6 to 12	15.2	15.8
	12 to 24	19.2	19.4
	24 to 36	21.6	21.2
	36 to 48	32.5	32.4

Date: 15 Feb 06			
Times: 1000 through 1330			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6	8.2	8.4
	6 to 12	12.8	12.7
	12 to 24	18.5	18.4
	24 to 36	9.2	9.5
	36 to 48	8.8	8.7
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6	8.7	8.9
	6 to 12	7.6	7.4
	12 to 24	8.5	8.6
	24 to 36	14.6	14.5
	36 to 48	22.4	22.5
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

Date: 16 Feb 06			
Times: 0900 through 1300			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6	8.9	8.8
	6 to 12	12.5	12.9
	12 to 24	19.5	19.4
	24 to 36	10.3	10.5
	36 to 48	8.9	9.2
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6	8.5	8.5
	6 to 12	7.8	7.9
	12 to 24	8.4	8.8
	24 to 36	14.3	14.8
	36 to 48	23.4	23.5
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

Date: 17 Feb 06			
Times: 0800 through 1640			
Probe location	**Layer, in.**	**AM Reading, %**	**PM Reading, %**
Wet area	0 to 6	8.5	8.4
	6 to 12	12.4	12.3
	12 to 24	19.3	19.2
	24 to 36	10.7	10.6
	36 to 48	8.8	8.7
Wooded area	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Open area	0 to 6	8.8	8.7
	6 to 12	8.2	7.9
	12 to 24	8.7	8.5
	24 to 36	14.9	14.4
	36 to 48	24.7	24.5
Calibration lanes	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		
Blind grid/moguls	0 to 6		
	6 to 12		
	12 to 24		
	24 to 36		
	36 to 48		

APPENDIX D. DAILY ACTIVITY LOG

Date, 06	No. of People	Area Tested	Status Start Time	Status Stop Time	Duration, min.	Operational Status	Operational Status Comments	Track Method	Pattern	Field Conditions
30 Jan	3	CALIBRATION LANES	1040	1325	165	INITIAL SETUP		RTS	LINEAR	FOGGY WET
30 Jan	3	CALIBRATION LANES	1325	1350	25	INITIAL SETUP		RTS	LINEAR	FOGGY WET
30 Jan	3	CALIBRATION LANES	1350	1715	205	INITIAL SETUP		RTS	LINEAR	FOGGY WET
31 Jan	3	CALIBRATION LANES	800	1340	340	INITIAL SETUP		RTS	LINEAR	MUDDY WINDY
31 Jan	3	CALIBRATION LANES	1340	1435	55	CALIBRATION		RTS	LINEAR	MUDDY WINDY
31 Jan	3	CALIBRATION LANES	1435	1545	70	COLLECTING DATA		RTS	LINEAR	MUDDY WINDY
31 Jan	3	CALIBRATION LANES	1545	1610	25	CALIBRATION		RTS	LINEAR	MUDDY WINDY
31 Jan	3	CALIBRATION LANES	1610	1700	50	DAILY START, STOP	EQUIPMENT BREAKDOWN	RTS	LINEAR	MUDDY WINDY
1 Feb	3	CALIBRATION LANES	745	950	125	DAILY START, STOP	EQUIPMENT SETUP	RTS	LINEAR	CLOUDY MUDDY
1 Feb	3	CALIBRATION LANES	950	1035	45	CALIBRATION		RTS	LINEAR	CLOUDY MUDDY
1 Feb	3	CALIBRATION LANES	1035	1205	90	COLLECTING DATA		RTS	LINEAR	CLOUDY MUDDY
1 Feb	3	CALIBRATION LANES	1205	1240	35	CALIBRATION		RTS	LINEAR	CLOUDY MUDDY
1 Feb	3	CALIBRATION LANES	1240	1340	60	BREAK/LUNCH		RTS	LINEAR	CLOUDY MUDDY
1 Feb	3	CALIBRATION LANES	1340	1445	65	CALIBRATION		RTS	LINEAR	CLOUDY MUDDY
1 Feb	3	BLIND TEST GRID	1445	1610	85	COLLECTING DATA		RTS	LINEAR	CLOUDY MUDDY
1 Feb	3	BLIND TEST GRID	1610	1640	30	CALIBRATION		RTS	LINEAR	CLOUDY MUDDY
1 Feb	3	BLIND TEST GRID	1640	1730	50	DAILY START, STOP	EQUIPMENT BREAKDOWN	RTS	LINEAR	CLOUDY MUDDY
1 Feb	3	MOGUL	755	945	110	DAILY START, STOP	EQUIPMENT SETUP	RTS	LINEAR	SUNNY MUDDY
2 Feb	3	MOGUL	945	1110	85	CALIBRATION		RTS	LINEAR	SUNNY MUDDY

Note: Activities pertinent to this specific demonstration are indicated in highlighted text.

Date, 06	No. of People	Area Tested	Status Start Time	Status Stop Time	Duration, min.	Operational Status	Operational Status Comments	Track Method	Pattern	Field Conditions
2 Feb	3	MOGUL	1110	1115	5	BREAK/LUNCH		RTS	LINEAR	SUNNY MUDDY
2 Feb	3	MOGUL	1115	1225	70	COLLECTING DATA		RTS	LINEAR	SUNNY MUDDY
2 Feb	3	MOGUL	1225	1305	40	BREAK/LUNCH		RTS	LINEAR	SUNNY MUDDY
2 Feb	3	MOGUL	1305	1700	235	COLLECTING DATA		RTS	LINEAR	SUNNY MUDDY
2 Feb	3	MOGUL	1700	1740	40	CALIBRATION		RTS	LINEAR	SUNNY MUDDY
2 Feb	3	MOGUL	1740	1805	25	DAILY START, STOP	EQUIPMENT BREAKDOWN	RTS	LINEAR	SUNNY MUDDY
2 Feb	3	MOGUL	755	1015	140	DAILY START, STOP	EQUIPMENT SETUP	RTS	LINEAR	SUNNY MUDDY
3 Feb	3	MOGUL	1015	1055	40	CALIBRATION		RTS	LINEAR	SUNNY MUDDY
3 Feb	3	MOGUL	1055	1220	85	COLLECTING DATA		RTS	LINEAR	SUNNY MUDDY
3 Feb	3	MOGUL	1220	1310	50	BREAK/LUNCH		RTS	LINEAR	SUNNY MUDDY
3 Feb	3	CALIBRATION LANES	1310	1350	40	COLLECTING DATA		RTS	LINEAR	SUNNY MUDDY
3 Feb	3	CALIBRATION LANES	1350	1430	40	CALIBRATION		RTS	LINEAR	SUNNY MUDDY
17 Feb	3	CALIBRATION LANES	1700	1845	105	DEMOBILIZATION		RTS	LINEAR	SUNNY MUDDY

Note: Activities pertinent to this specific demonstration are indicated in highlighted text.

APPENDIX E. REFERENCES

1. Standardized UXO Technology Demonstration Site Handbook, DTC Project No. 8-CO-160-000-473, Report No. ATC-8349, March 2002.

2. Aberdeen Proving Ground Soil Survey Report, October 1998.

3. Data Summary, UXO Standardized Test Site: APG Soils Description, May 2002.

4. Yuma Proving Ground Soil Survey Report, May 2003.

APPENDIX F. ABBREVIATIONS

APG	=	Aberdeen Proving Ground
ATC	=	U.S. Army Aberdeen Test Center
DMM	=	discarded military munitions
EM	=	electromagnetic
EMI	=	electromagnetic induction
ERDC	=	U.S. Army Corps of Engineers Engineer Research and Development Center
EST	=	Eastern Standard Time
ESTCP	=	Environmental Security Technology Certification Program
EQT	=	Army Environmental Quality Technology Program
IMU	=	inertial measurement unit
JPG	=	Jefferson Proving Ground
MEC	=	munitions and explosives of concern
NS	=	nonstandard
POC	=	point of contact
QA	=	quality assurance
QC	=	quality control
ROC	=	receiver-operating characteristic
RTK	=	real-time kinematic
RTS	=	Robotic Total Station
SERDP	=	Strategic Environmental Research and Development Program
USAEC	=	U.S. Army Environmental Command
UXO	=	unexploded ordnance
YPG	=	U.S. Army Yuma Proving Ground

APPENDIX G.   DISTRIBUTION LIST

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